



VSC-based HVDC Transmission Systems

POWER SYSTEM MODELLING AND CONTROL (EEEN40550)

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Outline

- Motivation
- Control p_{ac} , q_{ac} , v_{dc} , v_{ac}
- Frequency control
- Example



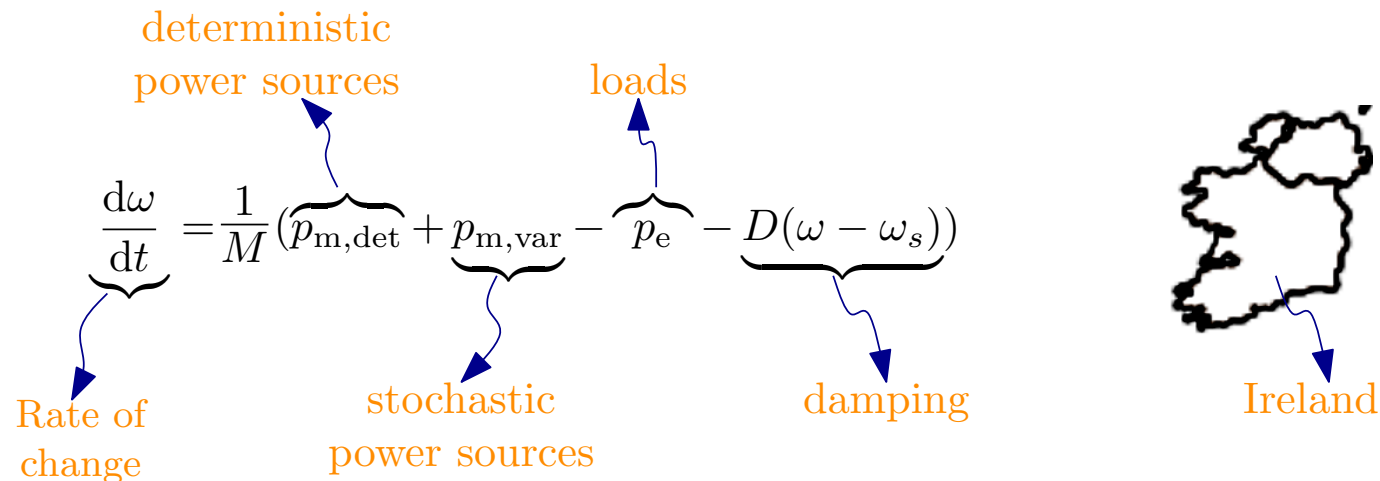
Motivation

- EU renewable targets
 - For 2020: 20% internally generated
 - For 2030: 27% collectively across Europe

- Electrical Grid Solution
 - Increase wind/solar production
 - Is it this clear cut?

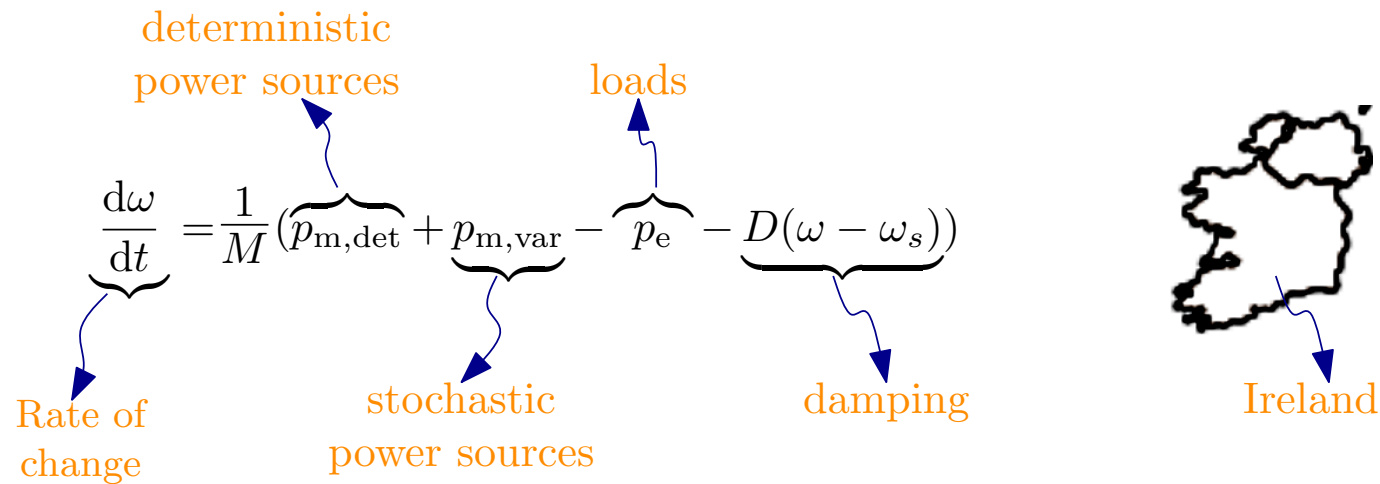
Issues

- Frequency dynamics in isolated AC grid, e.g., Ireland.

$$\underbrace{\frac{d\omega}{dt}}_{\text{Rate of change}} = \frac{1}{M} \left(\underbrace{p_{m,\text{det}}}_{\text{deterministic power sources}} + \underbrace{p_{m,\text{var}}}_{\text{stochastic power sources}} - \underbrace{p_e}_{\text{loads}} - \underbrace{D(\omega - \omega_s)}_{\text{damping}} \right)$$


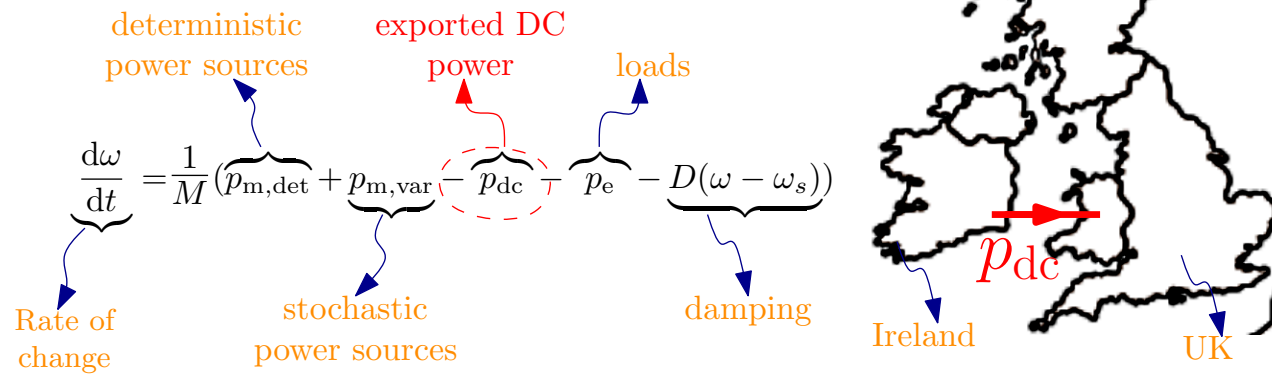
- $p_{m,\text{det}}$: deterministic power sources. Typically CO₂ **producing**, e.g., coal, oil, gas.
Highly certain power injection.
- $p_{m,\text{var}}$: stochastic power sources. Typically CO₂ **free**, e.g., wind, solar.
Uncertainty associated with power injection.

Issues

$$\underbrace{\frac{d\omega}{dt}}_{\text{Rate of change}} = \frac{1}{M} \left(\underbrace{p_{m,\text{det}}}_{\text{deterministic power sources}} + \underbrace{p_{m,\text{var}}}_{\text{stochastic power sources}} - \underbrace{p_e}_{\text{loads}} - \underbrace{D(\omega - \omega_s)}_{\text{damping}} \right)$$


- Frequency regulation must be tight.
 - ◇ Max. deviation = ± 1 Hz for Ireland
- Increasing $p_{m,\text{var}} \Rightarrow$ reduced ability to tightly regulate ω
 - \Rightarrow limit on clean energy penetration.
 - Limit largely dependent on M , the system inertia.

Add HVDC line



- Connect Ireland to UK with HVDC line.
- If too much $p_{m,var}$, export to UK. i.e. increase p_{dc}
- Also, if too little $p_{m,var}$, import from UK.
 \Rightarrow UK and Ireland can both increase stochastic renewable penetration.

Supergrid



Figure 1: One proposed “Supergrid” (only in planning stages)

- Potential renewable production varies temporally, geographically across Europe.
- HVDC based “Supergrid” planned for Europe.
- Allows continent-wide sharing of renewables.

Note: Supergrid vs large scale storage?

- Large-scale storage may in the future allow excess $p_{m, \text{var}}$ to be stored.
- Serious issues implementing large enough storage facilities. Technology constantly evolving however, e.g., Tesla large scale storage plans.
- Realistic future mix of HVDC & storage still **wide open research question!**
- HVDC posed as way of reaching large scale storage.
 - Norway has massive hydro reserves.
 - By connecting Norway to the Supergrid, could act as a vast battery for the European grid.
 - Sample article:
<http://spectrum.ieee.org/green-tech/wind/norway-wants-to-be-europes-battery>

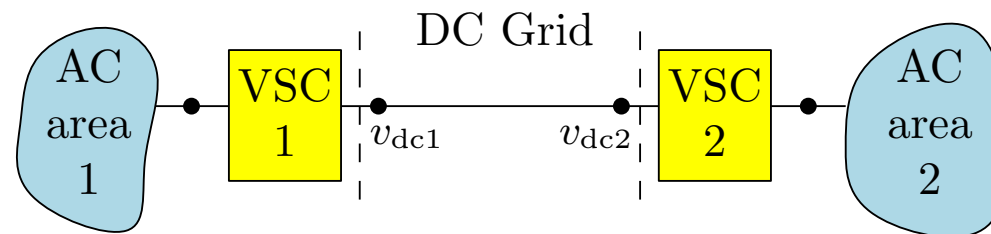


VSC vs. LCC technology

- Two technologies for implementing HVDC grids: VSCs and Line Commutated Converters (LCCs-see previous HVDC lecture)
- Advantages of VSC
 - Enables bi-directional power flows
 - Independent p_{ac} and q_{ac} control
 - Does not consume reactive power. LCC does.
- Typically most new HVDC lines are VSC.

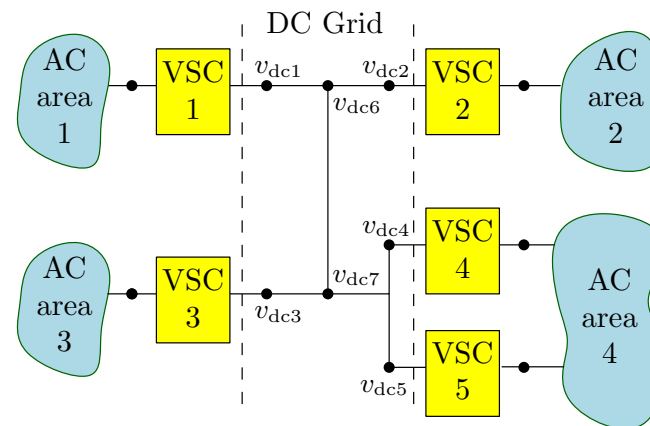
Configurations

- Most existing Back to Back HVDC links are point to point connections, i.e., the DC grid connects on two VSCs together.
 - East-West interconnector, Ireland.



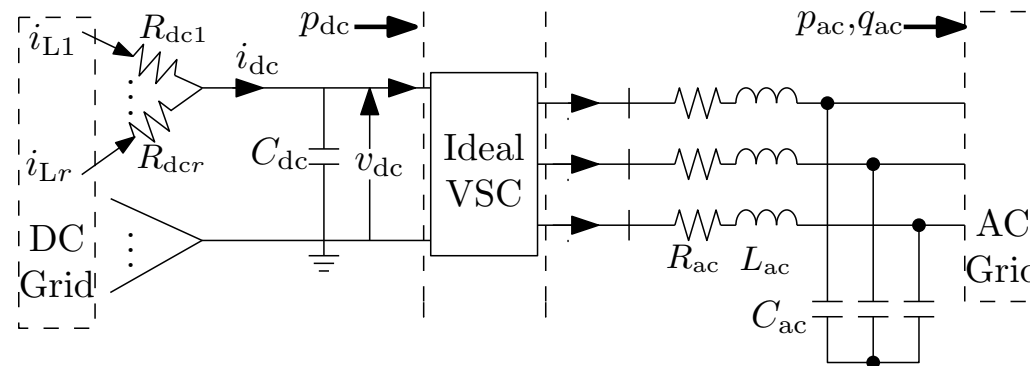
Configurations

- Multi-Terminal HVDC (MTDC) grids are grids where several DC lines connect to one VSC terminal.
- VSC technology enables the construction of flexible meshed MTDC grids. LCC MTDC grids less flexible due to uni-directional flows.
- First built in Nanao, China (2015), Northern European MTDC grid planned, as initial stage of Supergrid.



VSC between AC and DC grids

- Consider a single VSC in a MTDC grid



- Ideal VSC modelled as in FACTS lecture previously.
 - $p_{dc} = v_{dc} i_{dc}$
 - $p_{ac} = \frac{3}{2} (v_{ac,d} i_{ac,d} + v_{ac,q} i_{ac,q})$
 - $q_{ac} = \frac{3}{2} (-v_{ac,d} i_{ac,q} + v_{ac,q} i_{ac,d}) + Q_{C_{ac}}(t)$
 - $Q_{C_{ac}}$ is the reactive power corresponding to C_{ac}

DC dynamics

- $C_{dc} \frac{d}{dt} v_{dc} = i_{dc}$
 - where $i_{dc} = i_{L1} + i_{L2} + \dots + i_{Lr}$, and the VSC is connected via resistors R_{dc1}, \dots, R_{dcr} to r other DC voltage nodes.
 - Simple DC line models and VSC configurations are used here. More complex models of DC lines and VSC configurations are given in the book: “Multi-terminal Direct-Current Grids: Modelling, Analysis, and Control”, by Chauduri, Chauduri, Majumder, Yazdani, Wiley, 2014 (this is also what the modelling in this lecture is based on).

Phase Locked Loop (PLL)

- A PLL ensures that the VSC voltages and currents are synchronised with the system frequency.
- Allows outputs of VSC to be considered in synchronous d-q frame
- When PLL is “locked” into system frequency $v_{ac,q} = 0$

⇒ powers can now be represented as follows:

- $p_{ac} = \frac{3}{2} v_{ac,d} i_{ac,d}$

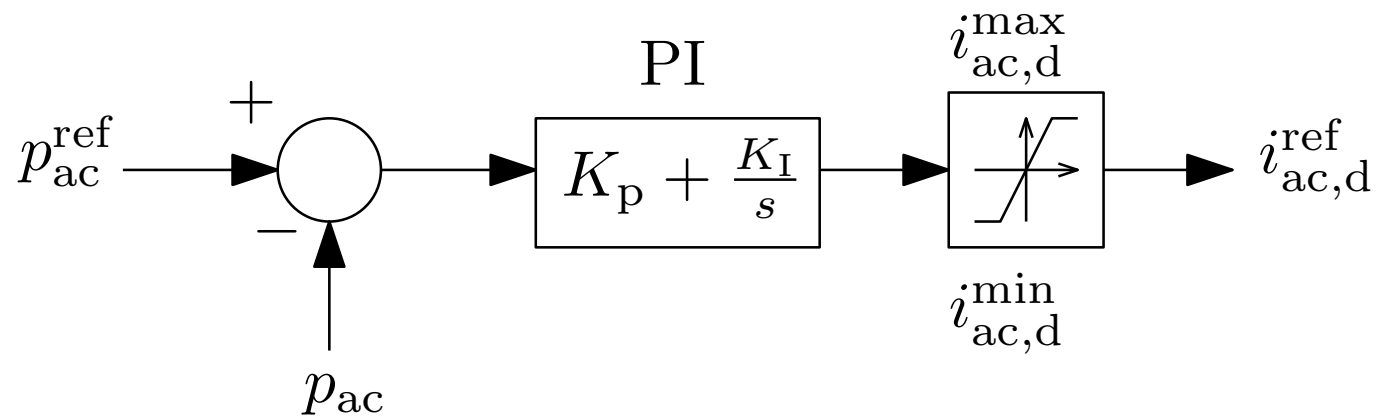
- $$q_{ac} = -\frac{3}{2} v_{ac,d} i_{ac,q} + \underbrace{\frac{3}{2} C_{ac} \omega v_{ac,d}^2}_{Q_{cac}}$$

$$= -\frac{3}{2} v_{ac,d} (i_{ac,q} - C_{ac} \omega v_{ac,d})$$

- Thus the PLL enables independent control of p_{ac} using $i_{ac,d}$, and q_{ac} using $i_{ac,q}$

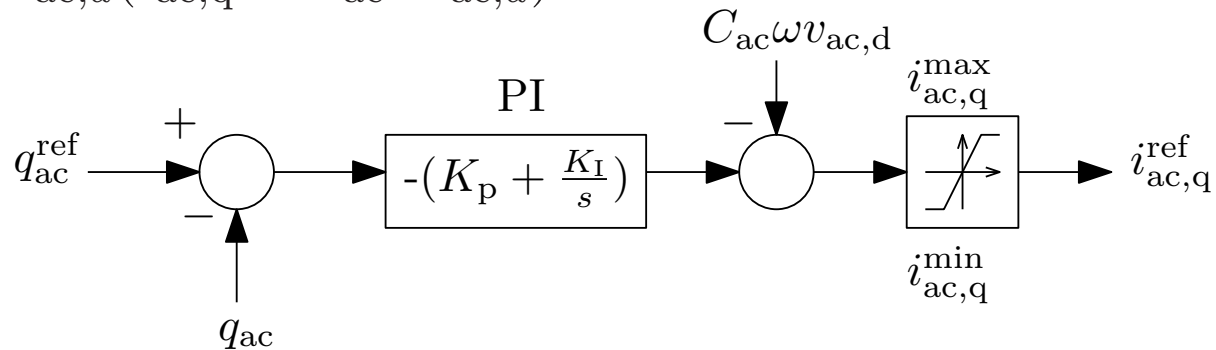
P and Q control

- $p_{ac} = \frac{3}{2} v_{ac,d} i_{ac,d}$; ($v_{ac,d}$ is generally kept near nominal value via voltage regulators)

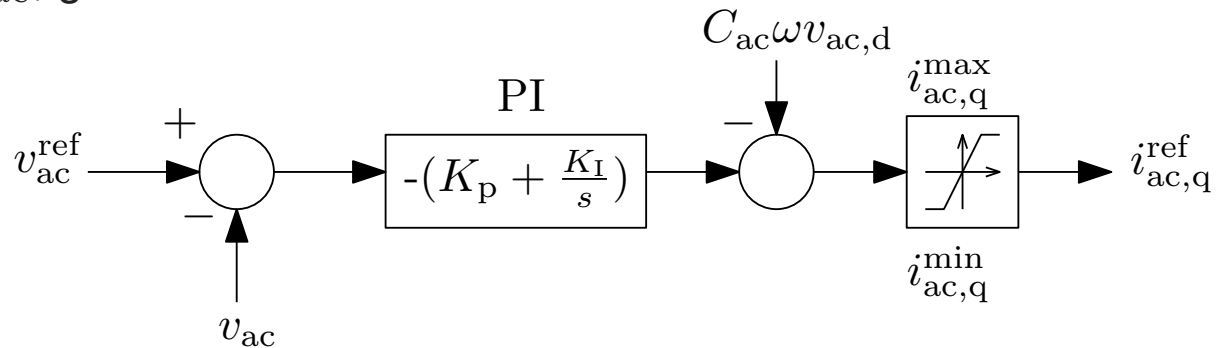


P and Q control

- $$q_{ac} = -\frac{3}{2}v_{ac,d}(i_{ac,q} - C_{ac}\omega v_{ac,d})$$



- $v_{ac,d} \propto q_{ac}$, gives



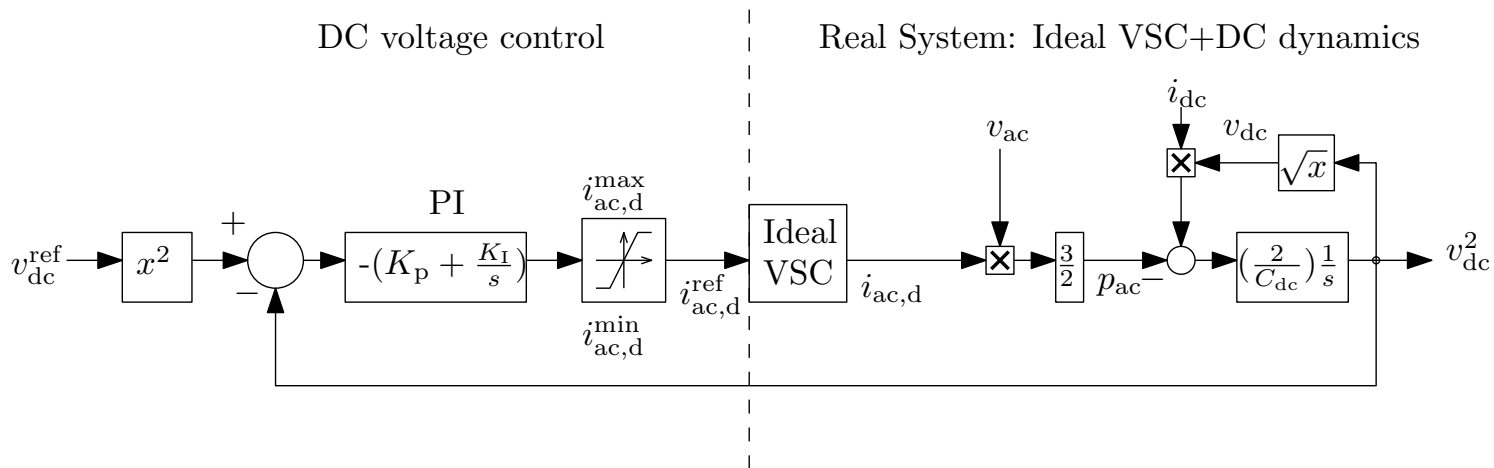
- Note, typically the $-C_{ac}\omega v_{ac,d}$ part of the controller can be left out.

Control of DC voltage

- Assuming minimal losses across VSC: $p_{dc} = p_{ac} = \frac{3}{2} v_{ac,d} i_{ac,d}$
- Energy in DC Capacitor: $\left(\frac{C_{dc}}{2}\right) \frac{dv_{dc}^2}{dt} = v_{dc} i_{dc} - \underbrace{\frac{3}{2} v_{ac,d} i_{ac,d}}_{p_{dc}=p_{ac}}$

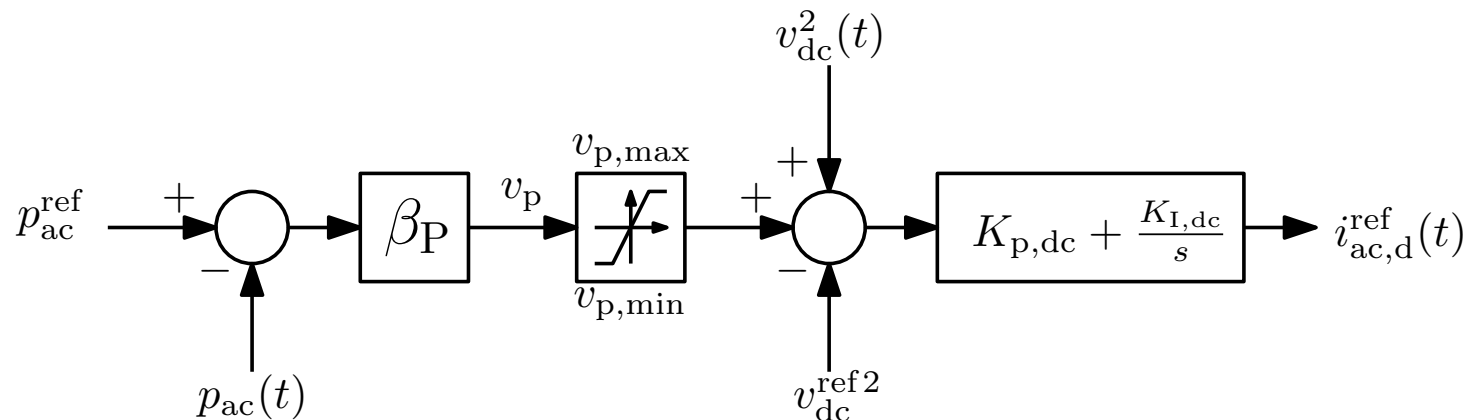
- Chain of influence:

$$v_{dc}^{ref} \rightarrow (v_{dc}^{ref2} - v_{dc}^2) \rightarrow i_{ac,d}^{ref} \rightarrow i_{ac,d} \rightarrow \frac{dv_{dc}^2}{dt} \rightarrow v_{dc}^2 \rightarrow v_{dc}$$



Combinations

- Use droop gains for regulation trade-offs.
- e.g., $i_{ac,d}$ can control both p_{ac} and v_{dc} . Dynamic trade-off of both given by:

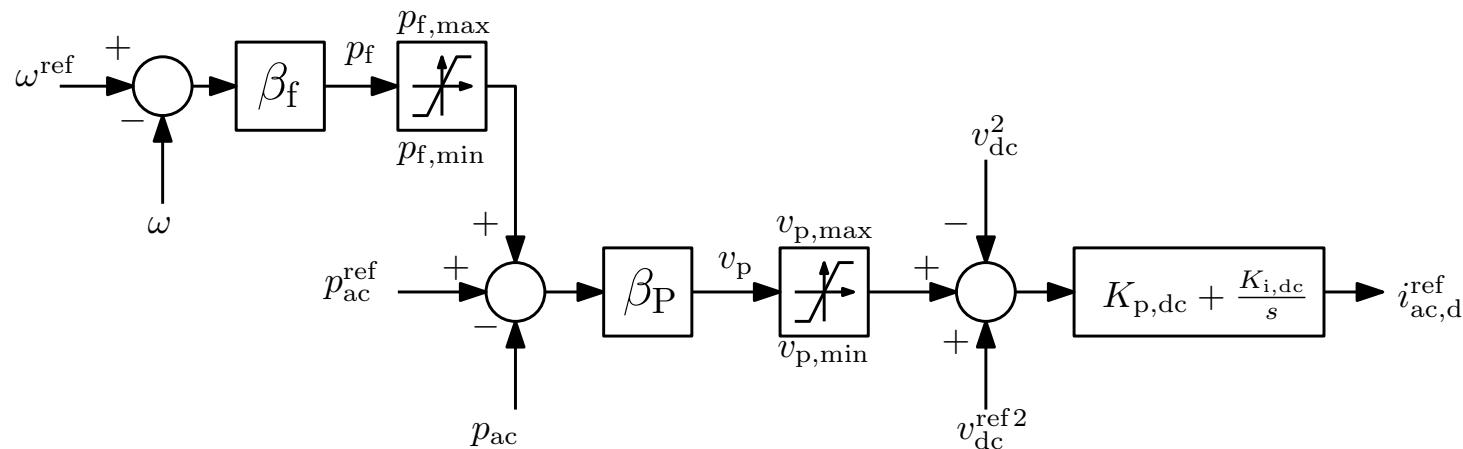


- β_P typically a gain. Determines importance of p_{ac} vs. v_{dc} regulation.
- Similar setup possible using $i_{ac,q}$ for q_{ac} and v_{ac} regulation.

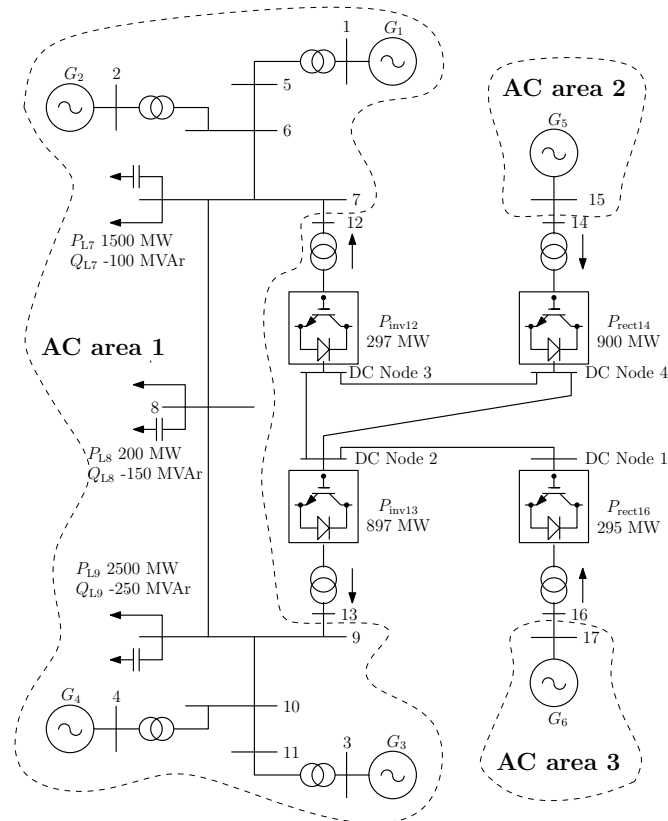
Dynamic frequency regulation

$$\frac{d\omega}{dt} = \frac{1}{M} (p_{m,\text{det}} + p_{m,\text{var}} - p_{\text{dc}} - p_e - D(\omega - \omega_s))$$

- System inertia M is provided by rotors (on generators, flywheels, etc).
- As DC interconnections displace machines with that provide inertia, system becomes more prone to large frequency swings.
- Desirable to emulate frequency response in DC power.
- Augment $i_{\text{ac},d}$ power control to respond to frequency deviations:

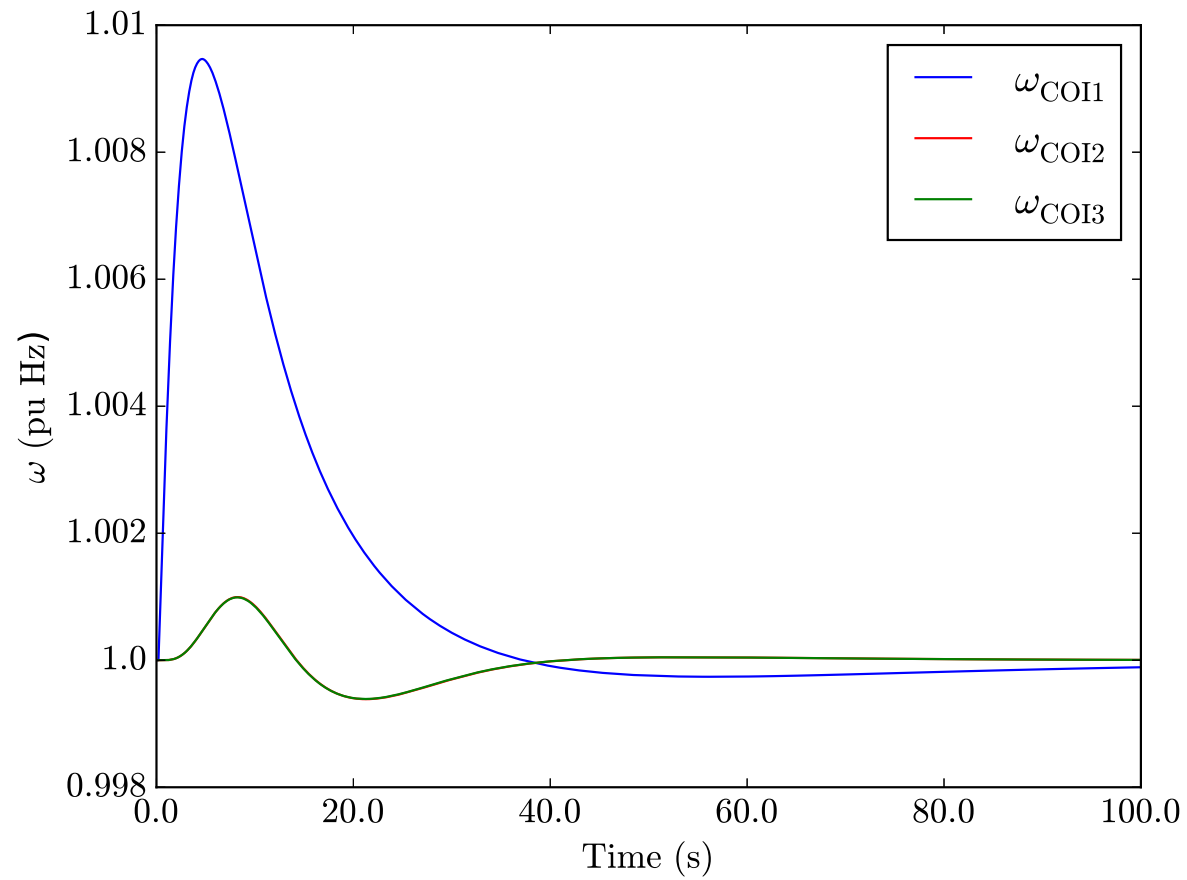


Dynamic frequency regulation example

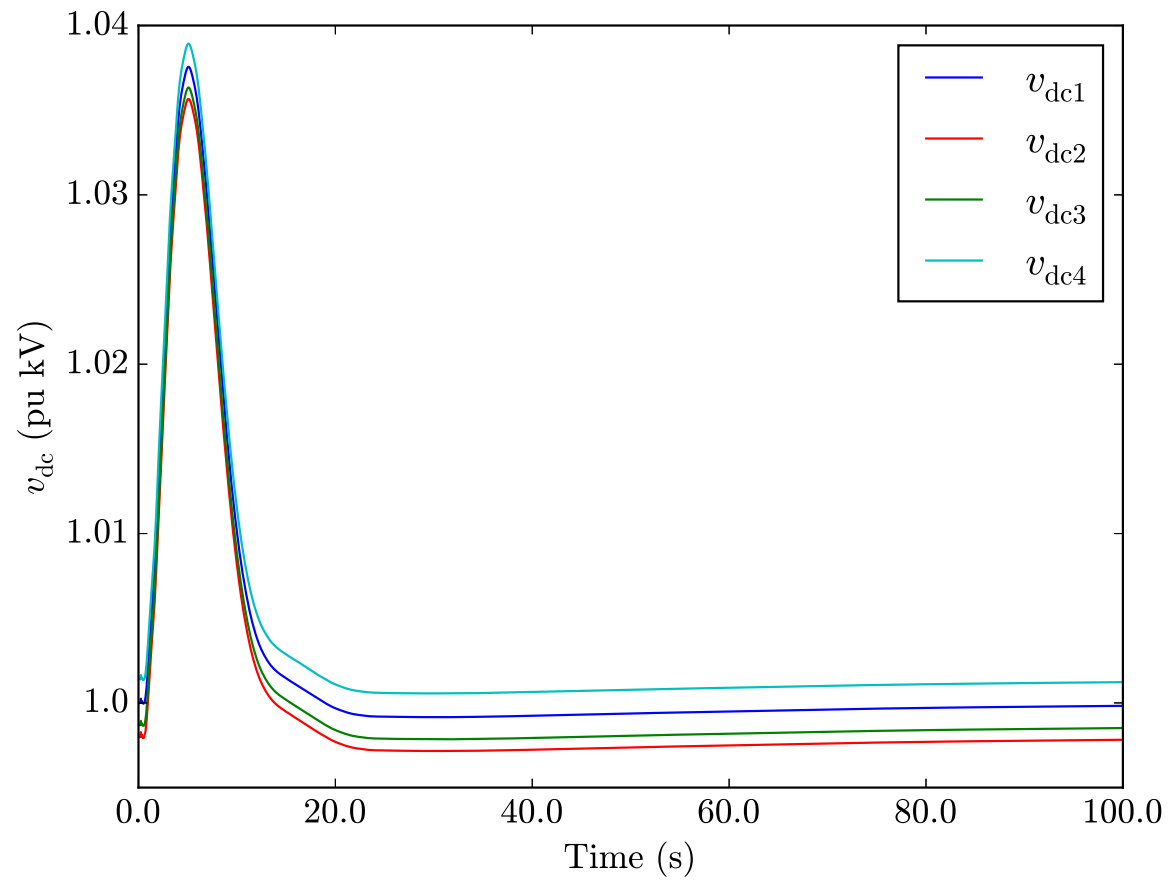


- Consider loss of load 8.

Dynamic frequency regulation example: Frequency



Dynamic frequency regulation example: DC voltages



Dynamic frequency regulation example: DC power deviations

